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# A Level-Set Immersed Boundary Method For Simulating Flows Around Cylinders In Tandem And Side-By-Side Arrangements

Radouan Boukharfane & Saad Benjelloun

Mohammed VI Polytechnic University (UM6P), MSDA Group, Benguerir, Morocco

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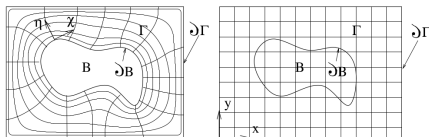
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**Immersed boundary method /  
Level set method**



## Immersed boundary method

Simulate flows on grids that do not conform to the shape of the boundaries

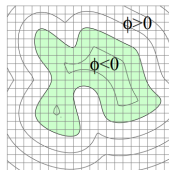


- Allow practitioners to side-step costly mesh generation process
- Arbitrary geometry is superimposed over a uniformly Cartesian grid
  - ✓ Apply a boundary closure rule to governing equations
  - ✓ Block-structure allows for simple AMR to resolve structures near boundary
- Simple, structured data layout with fixed spacing has favorable characteristics for HPC compared with e.g. unstructured approach
- Challenges
  - ✓ Reduction of order-of-accuracy at boundaries
  - ✓ **Numerical instability at boundaries since it can not capture smoothly the interface**
  - ✓ **Errors to the interpolation of kernels**

## Accurate Conservative Level Set Approach

- The interface is defined as zero level set of a distance function  $\phi(x, t)$  from the interface.
  - ✓ The level set scalar is assumed to be a signed distance function to the interface

$$\phi(x, t) = \begin{cases} -d & \text{inside the immersed solid} \\ 0 & \text{at the fluid-solid interface} \\ +d & \text{inside the fluid} \end{cases}$$



- The conservative level set approach defines the phase interface to be the  $\psi(x, t) = 0.5$  isosurface of

$$\psi(x, t) = \frac{1}{2} \left( \tanh \left( \frac{\phi(x, t)}{2\varepsilon} \right) + 1 \right),$$

- ✓  $\psi(x, t)$  is transported via the material evolution equation

$$\frac{\partial \psi}{\partial t} + \nabla \cdot (\psi \mathbf{u}) = 0.$$

## Accurate Conservative Level Set Approach

- Re-initialization is used to restore  $\psi$  to a hyperbolic tangent profile after transport (Chiodi and Desjardins, 2017; Sahut et al., 2020)

$$\frac{\partial \psi}{\partial \tau} = \nabla \cdot \left[ \frac{1}{4 \cosh^2 \left( \frac{\phi_{\text{map}}}{2\epsilon(\mathbf{x})} \right)} (\nabla \phi_{\text{map}} \cdot \mathbf{n}_{\text{FMM}} - \mathbf{n}_{\text{FMM}} \cdot \nabla \phi_{\text{map}}) \mathbf{n}_{\text{FMM}} \right]$$

with

- $\phi_{\text{map}}(\mathbf{x}, \tau) = \epsilon(\mathbf{x}) \log \left( \frac{\psi(\mathbf{x}, \tau)}{1 - \psi(\mathbf{x}, \tau)} \right)$  is the inverse of the conservative level set function.
- $\mathbf{n}_{\text{FMM}}$  is computed as

$$\mathbf{n}_{\text{FMM}}(\mathbf{x}, t) = \frac{\nabla \phi_{\text{FMM}}(\mathbf{x}, t)}{\|\nabla \phi_{\text{FMM}}(\mathbf{x}, t)\|}$$

with  $\phi_{\text{FMM}}$  a distance function computed from a Fast Marching Method algorithm

- The construction of  $\phi_{\text{FMM}}$  removes all oscillatory behaviors of  $\psi$  in the computation of normals.

**Numerical solver**



## Numerical solver

In each phase, the material properties are constant, which allows to write  $\varrho = \varrho_s$  in the solid immersed body, while  $\varrho = \varrho_f$  in the fluid, and  $\mu = \mu_s$  in the solid and  $\mu = \mu_f$  in the fluid.

$$\frac{\partial \varrho}{\partial t} + \mathbf{u} \cdot \nabla \varrho = 0$$

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\varrho} \nabla p + \frac{1}{\varrho} \nabla \cdot (\mu [\nabla \mathbf{u} + \nabla \mathbf{u}^T]),$$

- At the interface, the material properties are subject to a jump that is written  $[\varrho]_\Gamma = \varrho_f - \varrho_s$  and  $[\mu]_\Gamma = \mu_f - \mu_s$ .
- The velocity field is continuous across the interface,  $[\mathbf{u}]_\Gamma = 0$ .
- The existence of the pressure jump induces a discontinuity in the pressure at the interface  $\Gamma$ , and one can write

$$[p]_\Gamma = \sigma \kappa + [\mu]_\Gamma \mathbf{n}^\top \cdot \nabla \mathbf{u} \cdot \mathbf{n}.$$

- The solid–fluid coupling is achieved due to the Ghost-Fluid Method (GFM)



## Numerical solver

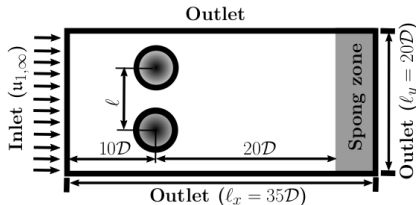
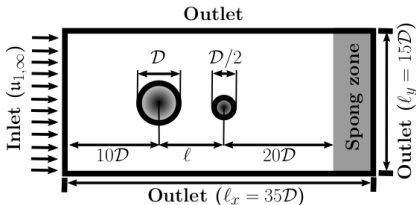
- Projection method based on fractional time steps developed by Chorin (1968) and improved by Kim and Moin (1985).
  - ✓ Fourth-order central scheme is used for the spatial integration
  - ✓ Third-order accurate semi-implicit Crank-Nicolson scheme is employed for time integration.
- Poisson equation is solved using the Livermore's `Hypre` library with the PCG (pre-conditioned conjugate gradient) method.

## Numerical results

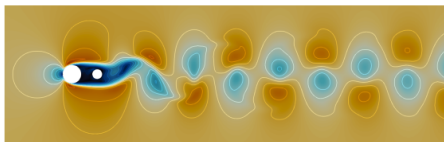


## Numerical results

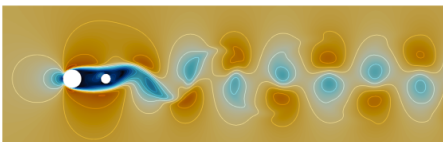
- The downstream cylinder is located at  $10D$  from the inflow boundary, while the upstream cylinder is positioned at  $10D$  from outgoing boundary.
- A sponge layer to damp out the possible reflection of pressure fluctuations at the outlet.
- $Re = \rho u_{1,\infty} D / \mu = 200$
- $1.5D \leq \ell \leq 4.0D$
- $\mathcal{N}_x \times \mathcal{N}_y = 800 \times 300$



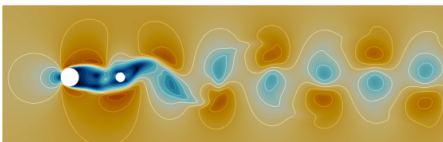
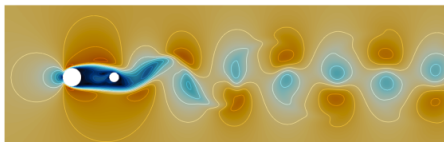
## Numerical results



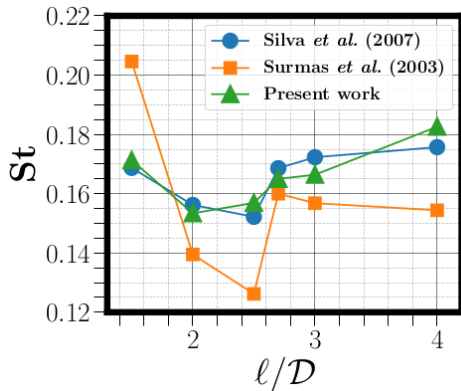
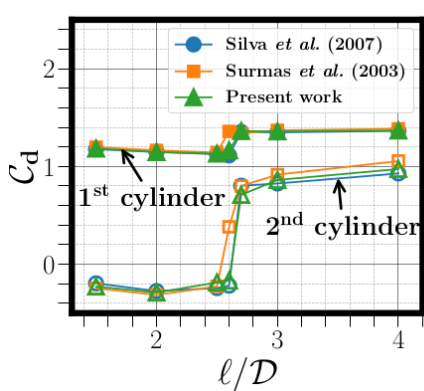
(a)  $l/D = 1.5$



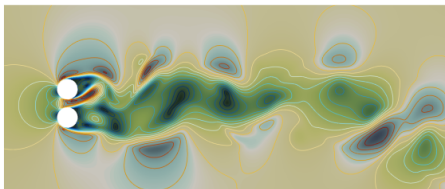
(b)  $l/D = 2.0$



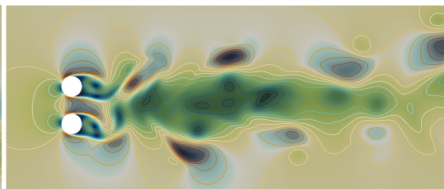
## Numerical results



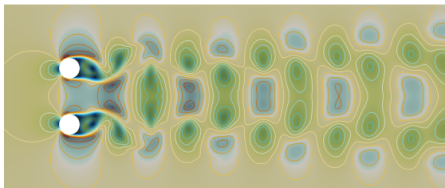
## Numerical results



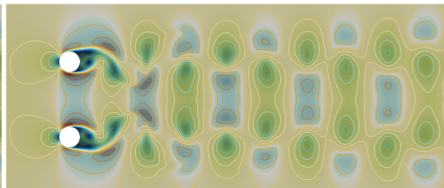
(a)  $l/D = 1.5$



(b)  $l/D = 2.0$

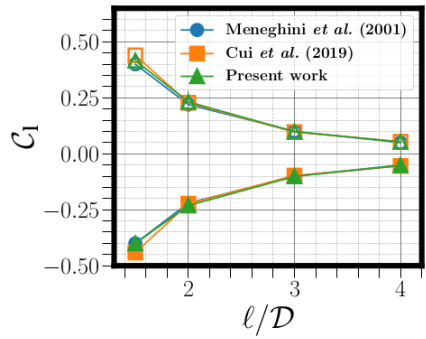
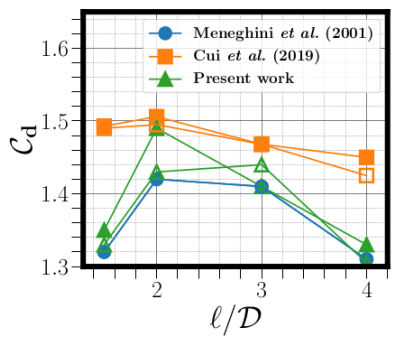


(c)  $l/D = 3.0$



(d)  $l/D = 4.0$

# Numerical results



## **Conclusion and perspectives**





## Conclusion and perspectives

- ➡ The accurate conservative level set with an important improvement of the modification of the re-initialization step is used for the two-way coupling of a fluid with rigid bodies.
- ➡ The performance of this method has been proven to correctly simulate flow over two cylinder in tandem and side-by-side arrangement
  - ✓ The results of the mean drag and lift coefficients and the Strouhal number were compared with other author's results.
- ➡ offer quite promising perspectives for future applications to more complex industrial problems.

Thank you for your kind attention 😊 !

Questions ?

Acknowledgments



## References

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