

Compressibility effects on homogeneous isotropic turbulence using Schur decomposition of the velocity gradient tensor

R. BOUKHARFANE, A. ER-RAIY & M. PARSANI

KING ABDULLAH UNIVERSITY OF SCIENCE AND TECHNOLOGY (KAUST)
EXTREME COMPUTING RESEARCH CENTER (ECRC)
ADVANCE ALGORITHM AND NUMERICAL SIMULATIONS LABORATORY (AANSLAB)
THUWAL, KINGDOM OF SAUDI ARABIA

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للعلوم والتقنية
King Abdullah University of
Science and Technology

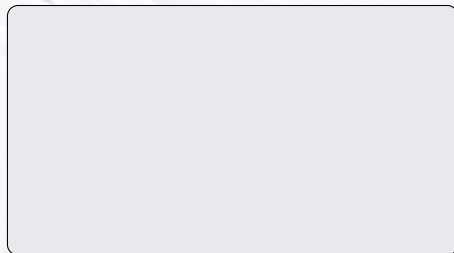
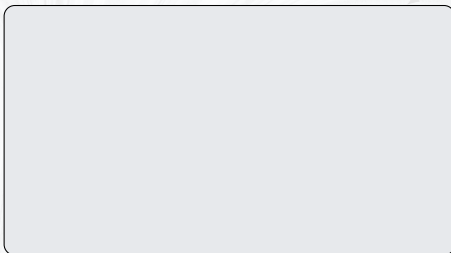


- ① MOTIVATION & PURPOSE
- ② NUMERICAL METHODS & DNS DATABASE
- ③ NUMERICAL RESULTS
- ④ CONCLUSION & PERSPECTIVES

Motivation

- Study of the velocity gradient tensor (VGT) $\mathcal{A}_{ij} = \partial u_i / \partial x_j$ in turbulent flows.
 - VGT contains all the necessary information
 - its role may be made explicit by taking the spatial gradient of the Navier-Stokes equations

$$\partial \mathcal{A} / \partial t + \mathbf{u} \cdot \nabla \mathcal{A} = -\mathcal{A}^2 - \mathcal{H} + \nu \nabla^2 \mathcal{A}, \text{ where } \mathcal{H}_{ij} = \partial^2 \mathcal{P} / \partial x_i \partial x_j$$



• Pope, S. B., Perry, A. E.
A general classification of three-dimensional turbulent velocity fields
Journal of Fluid Mechanics (1990)

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Study of the velocity gradient tensor



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graph TD; A[Study of the velocity gradient tensor] --> B[ ]; A --> C[ ]
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Cheng, M. S., Perna, A. P.

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Study of the velocity gradient tensor

Hermitian and skew-Hermitian decomposition approach

$$\mathcal{A} = \mathcal{S}^{\mathcal{A}} + \mathcal{\Omega}^{\mathcal{A}}, \quad \boldsymbol{\omega} = \nabla \times \mathbf{U}$$

alignment between the vorticity vector/scalar gradient and the eigenvectors of the strain rate tensor $\mathcal{S}^{\mathcal{A}}$



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Eigenvalue-based approach[¶]

$$\lambda_i^3 + P^{\mathcal{A}} \lambda_i^2 + Q^{\mathcal{A}} \lambda_i + R^{\mathcal{A}} = 0$$

$P^{\mathcal{A}} Q^{\mathcal{A}} R^{\mathcal{A}}$ invariants with the identities

$$P^{\mathcal{A}} = \sum_i \lambda_i, \quad Q^{\mathcal{A}} = \sum_{i < j} \lambda_i \lambda_j, \quad R^{\mathcal{A}} = \prod_i \lambda_i$$



¶ Chong, M. S., Perry, A. E.

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Purpose

- Unify eigenvalue-based approach and Hermitian/Skew-Hermitian approaches through a recently proposed Schur decomposition approach*

$$\mathcal{A} = \mathcal{B}^{\mathcal{A}} + \mathcal{C}^{\mathcal{A}}$$

- Use this decomposition to evaluate the influence of the compressibility on some statistical properties of the turbulent structures.

Conceptual Overview

- Schur decomposition $\mathcal{A} = \mathcal{U}\mathcal{T}\mathcal{U}^*$ which $\mathcal{T} = \mathcal{\Lambda} + \mathcal{N}$
 - $\mathcal{\Lambda}$ is diagonal matrix whose elements correspond to the eigenvalues of \mathcal{A}
 - \mathcal{N} is an upper triangular matrix that represents the non-normal part of \mathcal{A}
- Tensors of the additive decomposition $\mathcal{A} = \mathcal{B}^{\mathcal{A}} + \mathcal{C}^{\mathcal{A}}$ are defined as

$$\mathcal{B}^{\mathcal{A}} = \mathcal{U}\mathcal{\Lambda}\mathcal{U}^*$$

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Numerical solver

- Cartesian Navier-Stokes solver, three-dimensional, compressible, unsteady, viscous solver
 → Convective fluxes are discretized using a 7th accurate hybrid upwinded-WENO scheme[†].
 → Molecular fluxes are discretized using 8th order accurate centred difference scheme.
- Temporal integration is performed using 3rd accurate total variation diminishing RK scheme.

DNS database

Resolution	Re_λ	Ma_t	U'	$\langle \varepsilon / \rho \rangle$	$\Delta x / \eta$	\mathcal{L}_t / η	λ / η	Sk_3	Fl_3
512^3	100	0.12	0.54	0.11	1.18	151	19.80	-0.43	5.50
512^3	100	0.32	0.53	0.10	1.17	154	19.79	-0.45	5.64
512^3	100	0.50	0.53	0.10	1.15	154	19.59	-0.50	5.53
512^3	100	0.59	0.46	0.11	1.29	181	19.59	-0.51	5.94
512^3	100	0.73	0.45	0.09	1.35	175	19.37	-0.71	6.10
512^3	100	0.89	0.45	0.07	1.41	172	19.05	-1.18	8.81



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Estimate of the non-normality effects

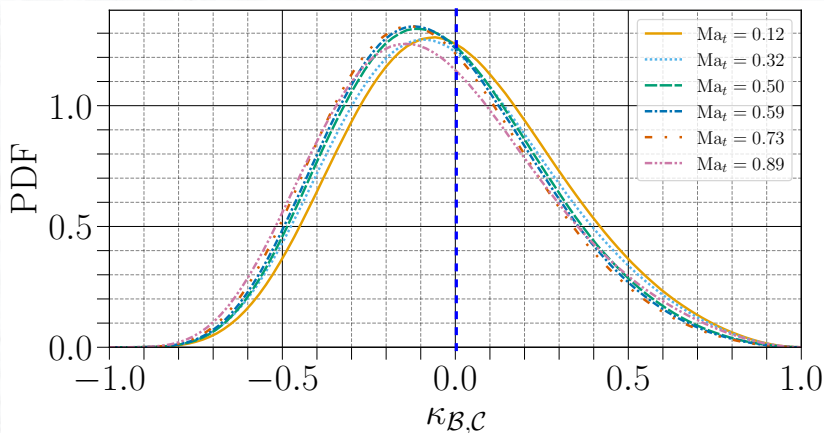
Use of standardized difference to understand when the non-normal effects are significant

$$\kappa_{\mathcal{B},\mathcal{C}} = \frac{\|\mathcal{B}\| - \|\mathcal{C}\|}{\|\mathcal{B}\| + \|\mathcal{C}\|}.$$

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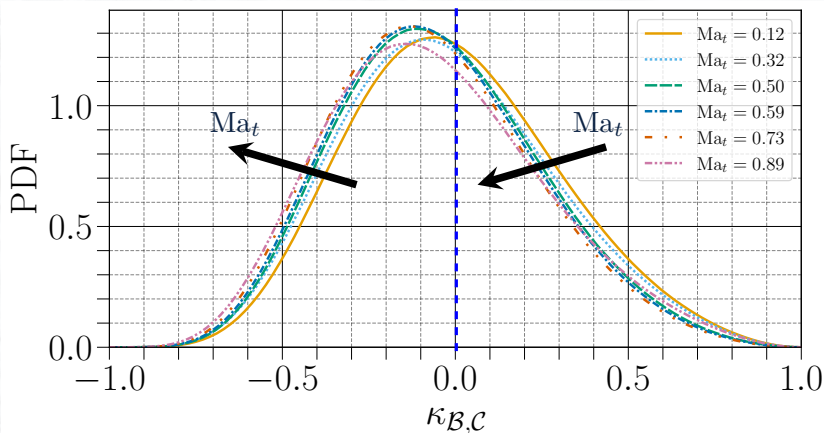
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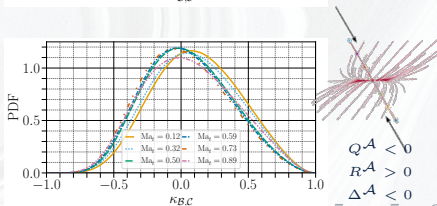
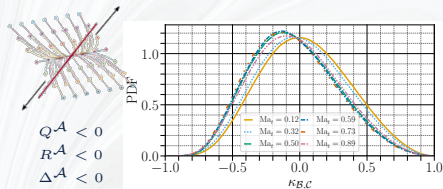
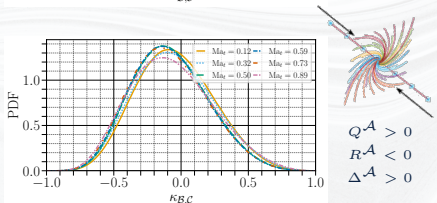
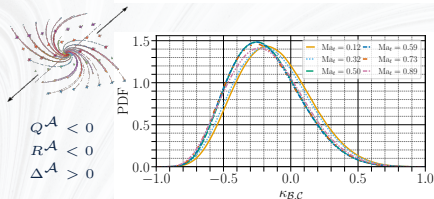
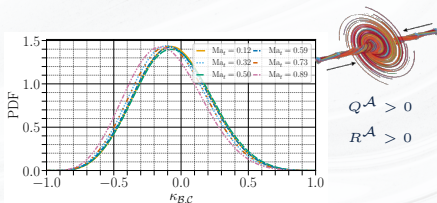
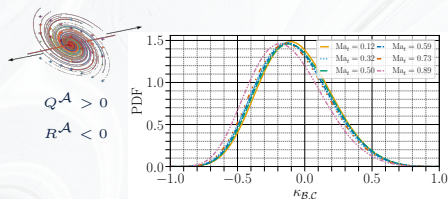
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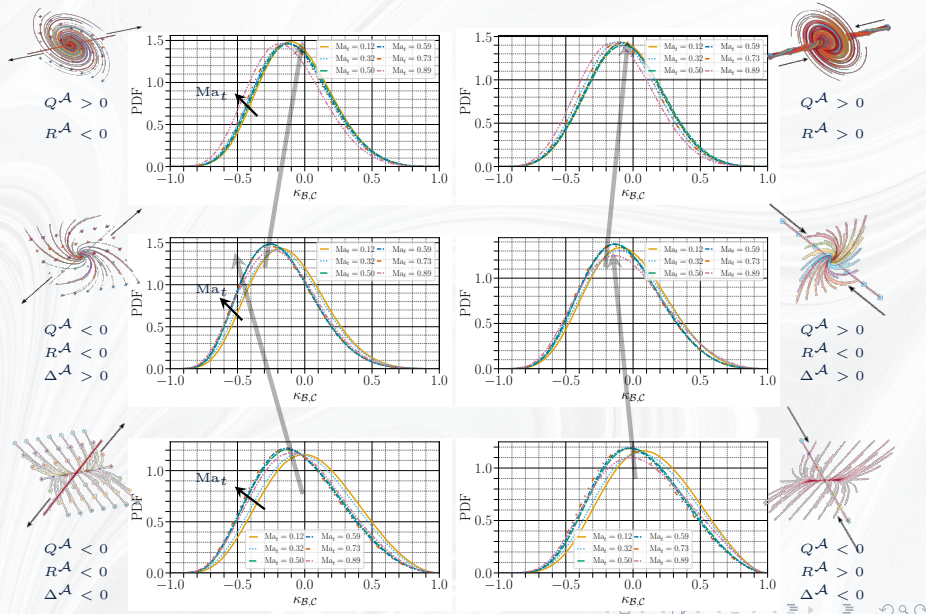
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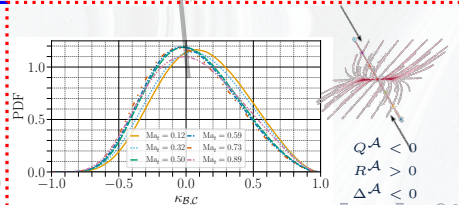
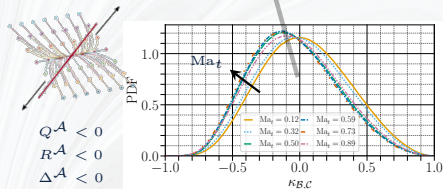
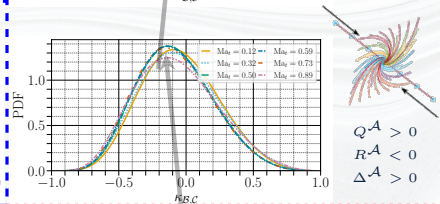
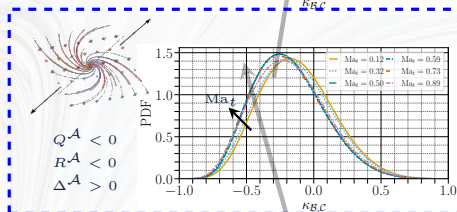
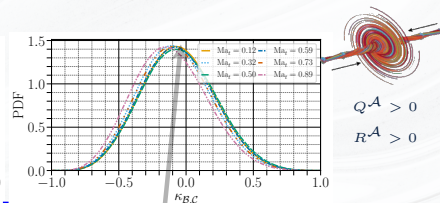
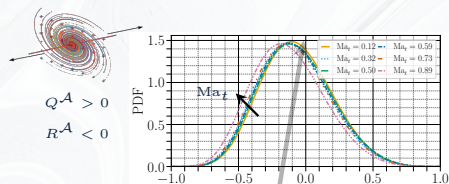
NUMERICAL RESULTS



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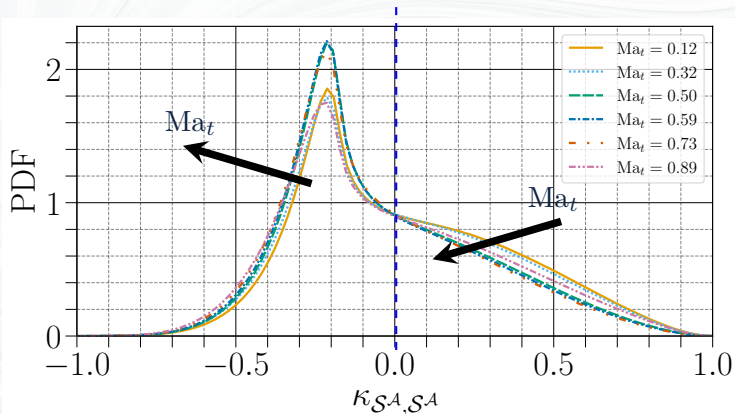
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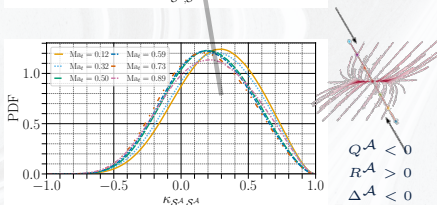
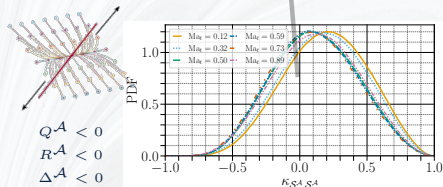
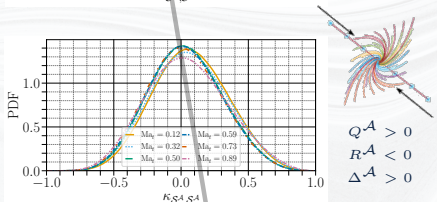
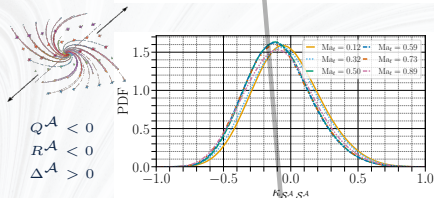
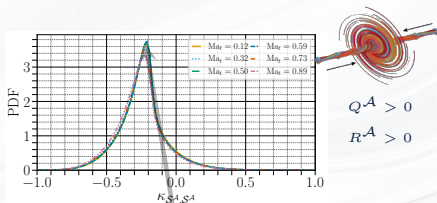
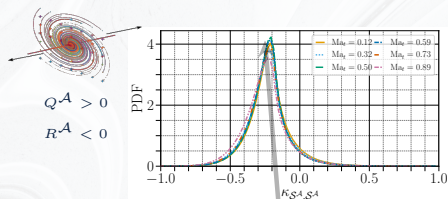
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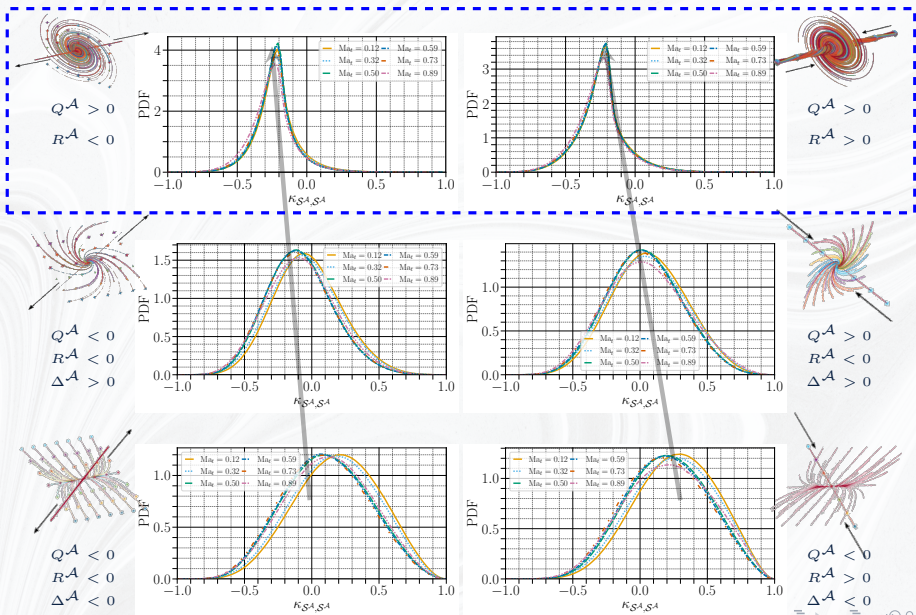
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Intermediate eigenvalue parameter

Normalization of the intermediate eigenvalue parameter of Lund* $e_{\mathcal{A}} = \frac{3\sqrt{6}R^{S^{\mathcal{A}}}}{(-2Q^{S^{\mathcal{A}}})^{3/2}}$

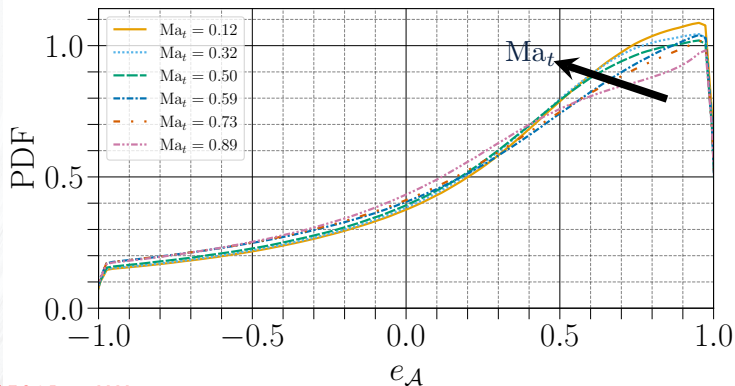


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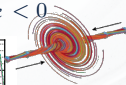
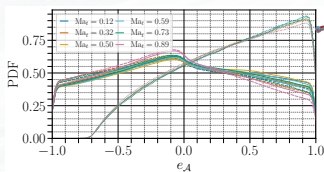
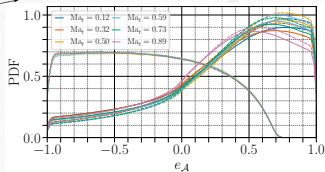
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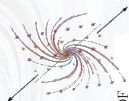
solid lines: all data | dashed lines: $\kappa_{SB,SC} > 0$ | dotted lines: $\kappa_{SB,SC} < 0$



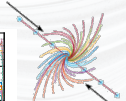
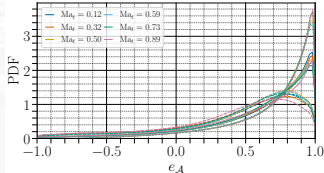
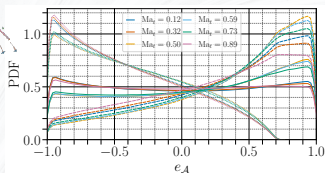
$Q^A > 0$
 $R^A < 0$



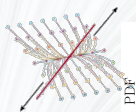
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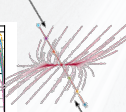
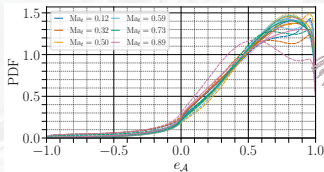
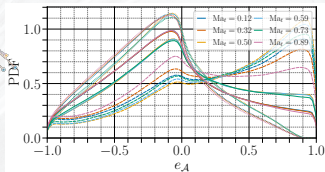
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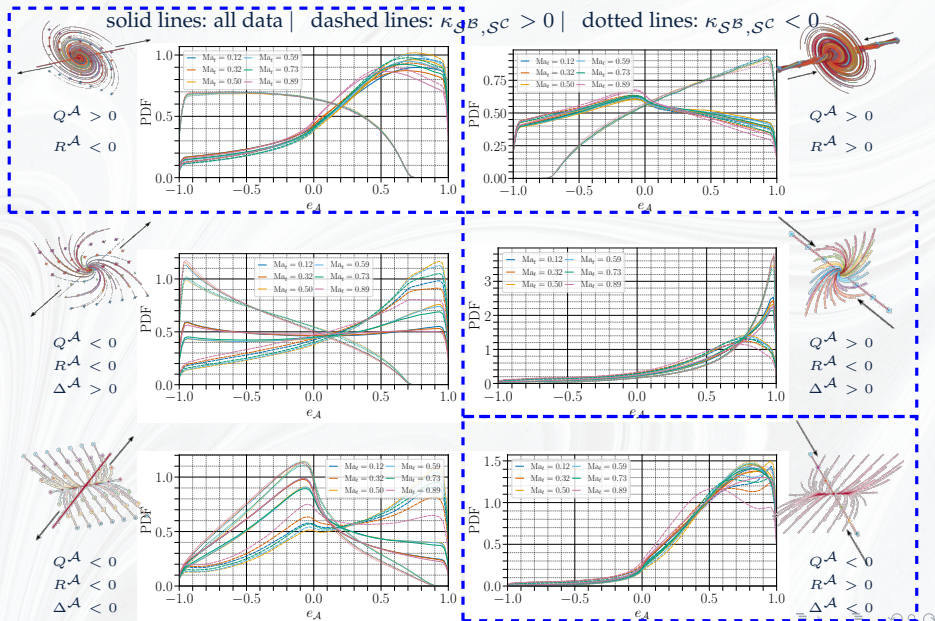


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Conclusion

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- The results clarify the way in which the different topology in different parts of $Q^{\mathcal{A}} - R^{\mathcal{A}}$ space affect the kinematics and dynamics of the flow.
- Compressibility show some noticeable effects when disaggregating normal and non-normal effects.

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Perspectives

- The next stage is to revisit some of the modeling approaches that already exist and to see if we can develop them in a more effective fashion using this approach.
- Moving beyond the HIT test case.

Thanks for your attention

Acknowledgments



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